



State-of-the-Art Reactor Consequence Analyses (SOARCA) Project: Sequoyah Uncertainty Analysis Methods and Insights

PSAM 14

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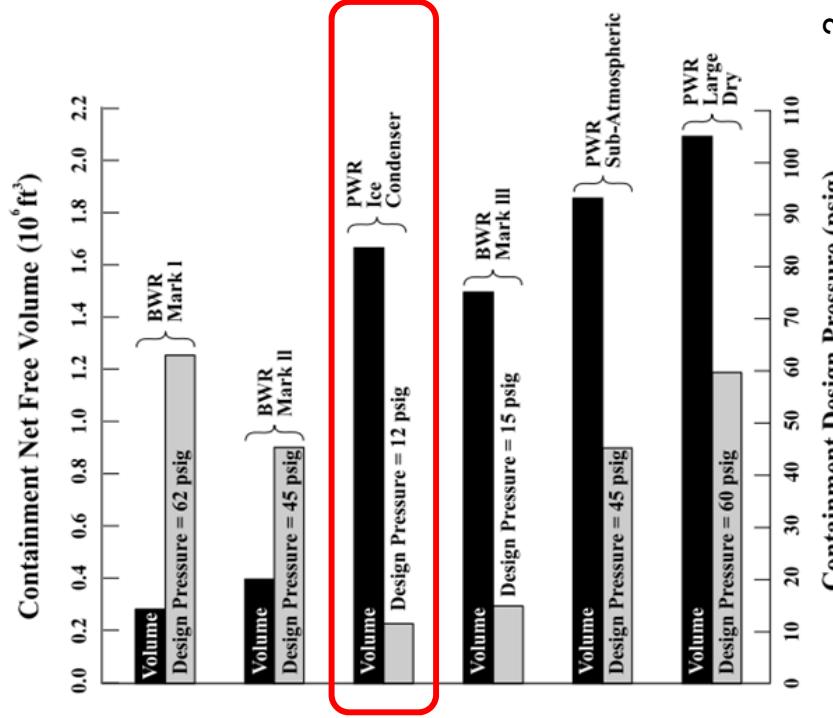


Outline

- Objectives and Overview of Short-Term Station Blackout (STSBO) Uncertainty Analysis (UA) for Sequoyah Nuclear Plant
- Uncertain Parameters Included in Study
- Severe Accident Progression and Release Results and Observations
- Summary and Next Steps

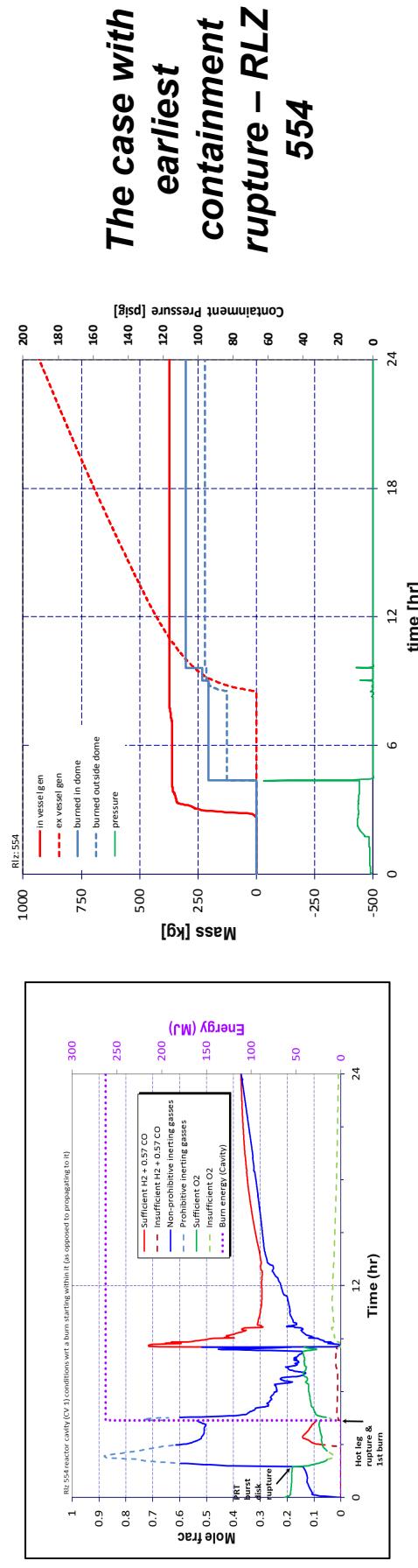


Objectives and Scope

- SOARCA goals and objectives
 - Develop body of knowledge on the realistic outcomes of severe reactor accidents
 - Incorporate state of the art modeling (MELCOR/MACCS)
 - Scope of Sequoyah analyses
 - Limited to station blackouts (SBOs)
 - Focused on issues unique to ice condenser containment and hydrogen challenges
 - Relatively low design pressure and smaller volume leads to potential susceptibility to early failure from hydrogen combustion in a station blackout
 - PWR Sub-Atmospheric
 - PWR Large Dry
- 
- The chart displays two sets of data series for PWR and BWR containment designs. The Y-axis represents Containment Net Free Volume in units of 10^6 ft^3 , ranging from 0.0 to 2.2. The X-axis represents Containment Design Pressure in psig, ranging from 0 to 110. The legend indicates that dark grey bars represent Volume and light grey bars represent Design Pressure. For PWR, there are three data points: Mark I (Volume ~0.6, Design Pressure = 12 psig), Mark III (Volume ~1.8, Design Pressure = 15 psig), and Sub-Atmospheric (Volume ~2.0, Design Pressure = 45 psig). For BWR, there are two data points: Mark II (Volume ~0.8, Design Pressure = 45 psig) and Mark I (Volume ~1.8, Design Pressure = 62 psig). A red box highlights the PWR Sub-Atmospheric and PWR Large Dry data points.
- | Containment Type | Design Pressure (psig) | Volume (10^6 ft^3) |
|---------------------|------------------------|--------------------------------|
| PWR Sub-Atmospheric | 45 | ~2.0 |
| PWR Large Dry | 62 | ~1.8 |
| PWR Mark III | 15 | ~1.8 |
| PWR Mark I | 12 | ~0.6 |
| BWR Mark II | 45 | ~0.8 |
| BWR Mark I | 62 | ~1.8 |

Overview of Sequoyah STSBO UA

- Integrated UA focused on unmitigated STSBO scenario
- Input parameter uncertainty propagated in a two-step Monte Carlo process, using 567 (out of 600) samples
- The UA results were examined in detail using both quantitative and qualitative approaches, such as phenomenological analysis of individual realizations.





Overview (continued)

- Four regression techniques were used to identify input parameters contributing to key accident progression characteristics and public health impacts.

Cesium Regression Table

		Sceenph_Fuel_Results_R2_1a.spg Data_Results_Final.xlsx									
		Bank Regression			Qualitative			Recursive Partitioning		MARS	
Final R ²		R ² contr.	SMC	S _i	T _i	S	T	0.51	0.77	0.77	
Input		0.40		0.77							
prSS_Vtype	0.26	0.53	0.32	0.56	0.58	0.56	0.41	0.41	0.76	0.280	0.294
Cycle	0.01	0.15	0.04	0.10	0.01	0.02	0.21	0.21	0.21	0.051	0.019
Rupture	0.05	0.22	0.01	0.14	—	—	0.01	0.01	0.01	0.016	0.051
Cu_Melt_T	0.02	0.15	0.02	0.27	0.02	0.40	0.01	0.01	0.30	0.013	0.205
Shape_Fact	0.04	0.21	—	—	0.00	0.00	0.00	0.00	0.00	0.010	0.000
Ox_Model	0.01	0.09	0.01	0.16	—	—	0.00	0.00	0.00	0.004	0.039
Fuel_Pressure	—	—	0.00	0.02	—	—	0.01	0.01	0.01	0.002	0.005
Scal_Open_A	0.01	-0.07	0.00	0.01	—	—	0.00	0.00	0.00	0.002	0.004
Sum_Dif	0.00	0.07	0.00	0.02	—	—	0.01	0.01	0.01	0.001	0.006

* highlighted if main contribution larger than 0.02 or conjoint contribution larger than 0.1

- A stability analysis was performed for the result metrics of interest (e.g., cesium and iodine release to the environment) using a bootstrapping method, to gain an understanding of the level of convergence in the statistical results

MELCOR Model Parameters

Sequence Related Parameters
Primary safety valve stochastic number of cycles until failure-to-close
Primary safety valve open area fraction after failure
Secondary safety valve stochastic number of cycles until failure-to-close
Secondary safety valve open area fraction after failure
In-Vessel Accident Progression
Melting temperature of the eutectic formed from fuel and zirconium oxides
Oxidation kinetics model
Ex-Vessel Accident Progression
Lower flammability limit hydrogen ignition criterion for an ignition source in lower containment
Containment rupture pressure
Barrier seal open area
Barrier seal failure pressure
Ice chest door open fraction
Particle dynamic shape factor
Time within the Fuel Cycle
Time-in-cycle (Beginning, Middle, End-of-Cycle: BOC, MOC, EOC)



MACCS

Uncertain Parameter Groups

Deposition

- Wet Deposition
- Dry Deposition Velocities

Dispersion

- Crosswind Dispersion Linear Coefficient
- Vertical Dispersion Linear Coefficient
- Time-Based Crosswind Dispersion Coefficient

Early Health Effects

- Threshold Dose
- Lethal Dose to 50% of population
- Hazard Function Shape Factor

Shielding Factors

- Groundshine Shielding Factors*
- Inhalation Protection Factors*
- Emergency Response

Latent Health Effects

- Dose and Dose Rate Effectiveness Factor
- Lifetime Cancer Fatality Risk Factors
- Long Term Inhalation Dose Coefficients
- Evacuation Delay*
- Evacuation Speed*
- Hotspot Relocation Time and Dose Criteria
- Normal Relocation Time and Dose Criteria
- Keyhole Forecast Time
- Aleatory Uncertainty
- Weather Trials

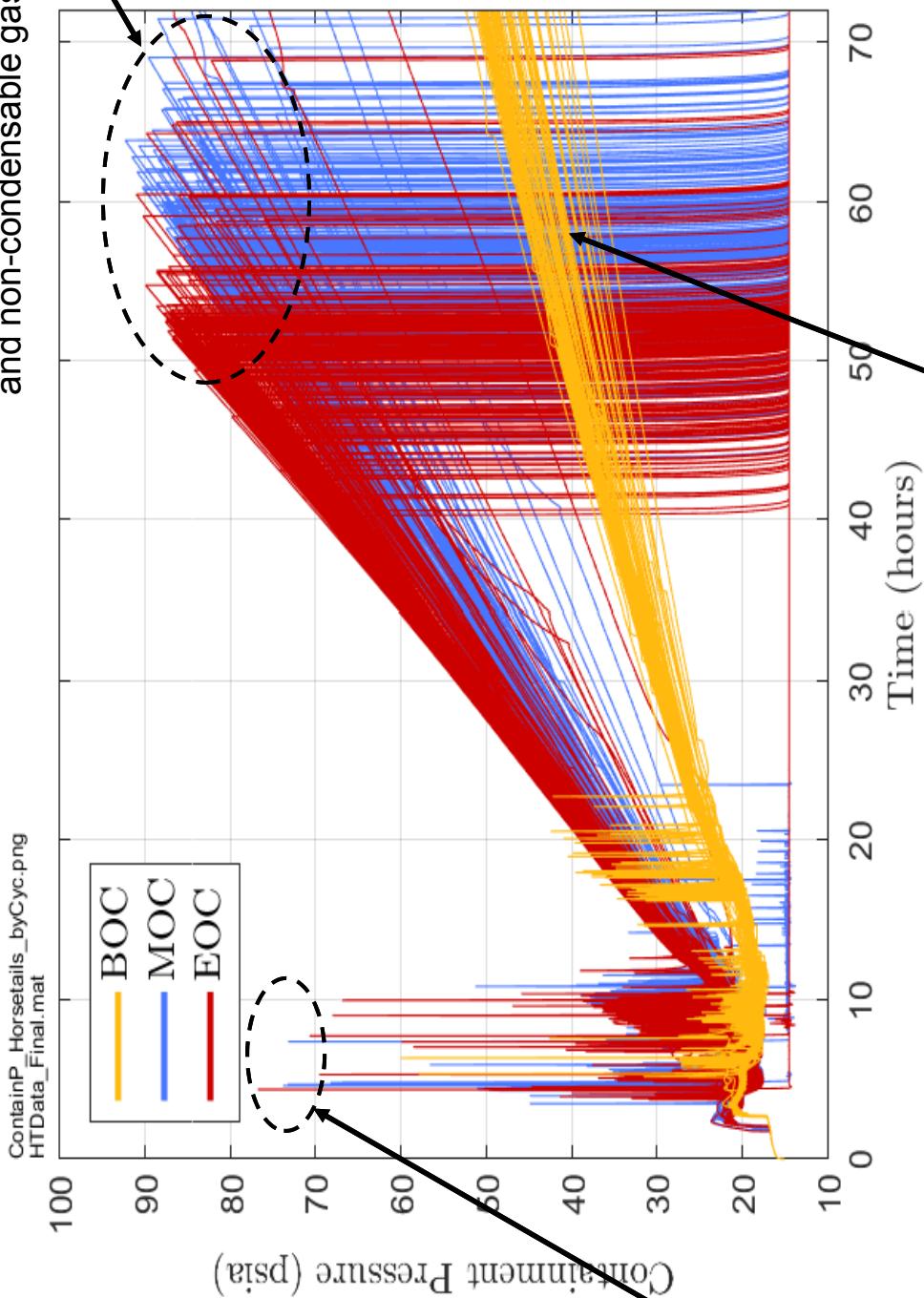


Containment Failure Outcomes

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Protecting People and the Environment

Long-term containment over-pressurization failure due to prolonged steam production and non-condensable gas generation

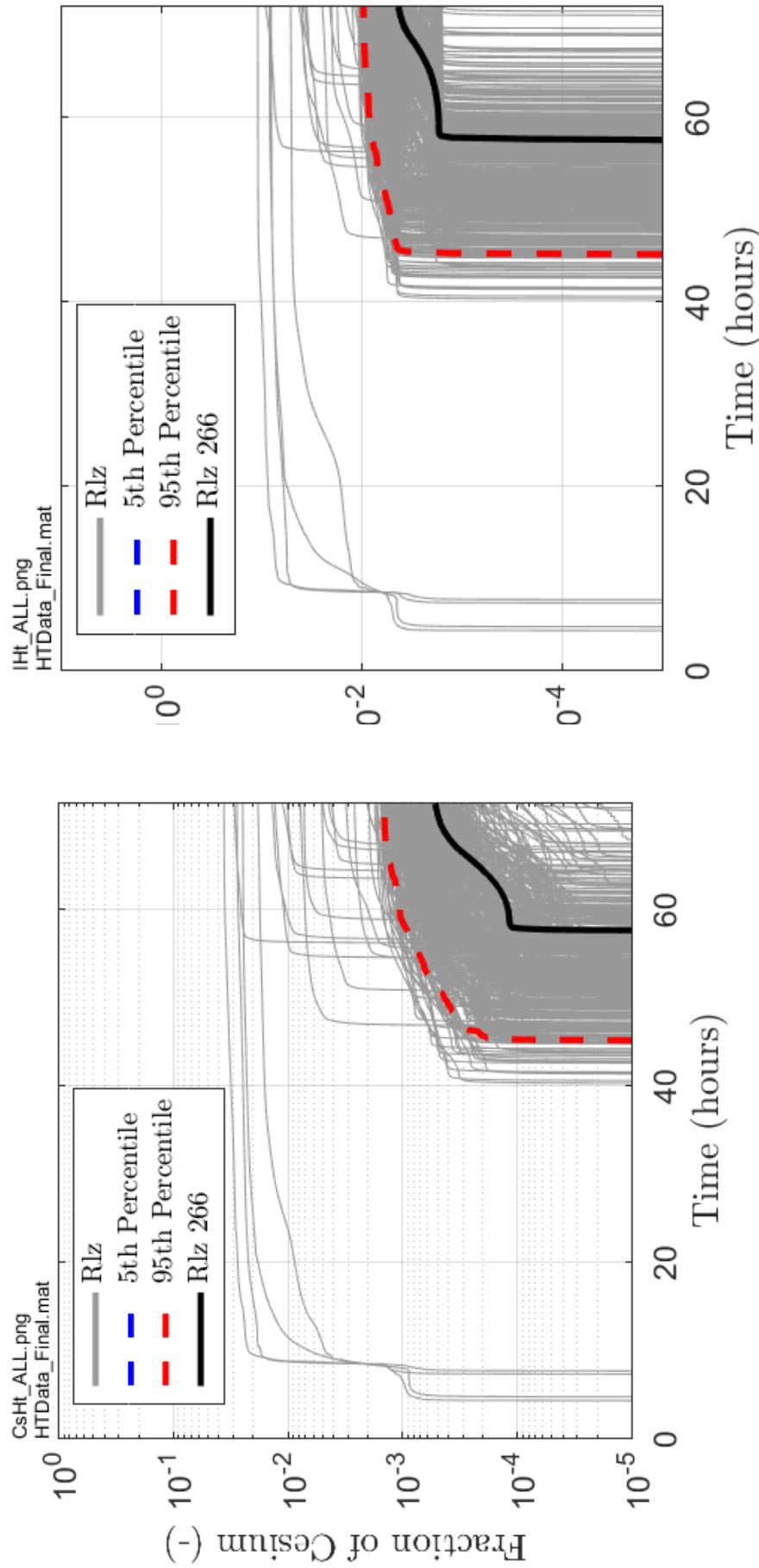


Early containment overpressure failures due to sufficiently large burns in containment

No BOC cases exhibit long-term overpressure failure before 72 hours



Cesium (left) and Iodine (right) Environmental Release Fraction Horsetails from STSBO UA





Severe Accident Progression STSBO High Level General Observations

- Consequences strongly (and intuitively) affected by *early vs. late* containment failure. Early containment failure dominated by hydrogen combustion, and late containment failure results mainly from ex-vessel phenomena (e.g., CCI)
- Early containment failures occur *only on the first hydrogen burn* (subsequent burns do not challenge containment integrity)
- Protracted safety valve (SV) cycling produces *lower in-vessel hydrogen* by the time of first burn
- Pressurizer SV failure to close (with large open area) results in greater hydrogen production and transport to the containment prior to the first burn, which increases the potential for early containment failure
- Late containment failures generally have reduced source term release benefiting from gravitational settling



Summary and Next Steps

- SOARCA Sequoyah analysis confirmed insights from previous analyses and yielded some new insights too
 - MACCS offsite consequence analyses will be discussed in session Th14, Paper 211
- Will be published as NUREG/CR-7245 within the next month, and available through NRC's website www.nrc.gov
- NRC is developing a NUREG report that will summarize the insights from all three SOARCA UAs completed